# TRI-AXIAL ELLIPSOIDS AS MODELS FOR MACROMOLECULES IN SOLUTION: PROCEDURES FOR NUMERICAL INVERSION OF THE SHAPE FUNCTIONS LEADING TO A STABLE UNIQUE SOLUTION 

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#### Abstract

Two FORTRAN IV algorithms are given for determining the two axial ratios of a macromolecule (as modelled by a tri-axial ellipsoid) from its hydrodynamic parameters. The first involves a simple graphical inversion procedure of the volume independent $\Lambda$ and $R$ functions but can only be applied to a restricted range of macromolecules. The second algorithm is more general and involves an $R$-function constrained non-linear least squares fit to birefringence decay data. $\begin{array}{lll}\text { Macromolecular shape } & \text { Tri-axial ellipsoid } \\ \text { Constrained minimization } & \text { Graphical intersection method }\end{array}$


## 1. INTRODUCTION

In an earlier communication [1] an algorithm was presented for evaluating the hydrodynamic parameters of a macromolecule (as modelled by a general tri-axial ellipsoid) from given values of its axial ratios. The development of an algorithm for performing the reverse operation [viz. evaluation of the two axial ratios $(a / b, b / c)$ of the ellipsoid of semiaxes $a \geqslant b \geqslant c]$ is not so simple. The difficulties derive from the fact that, although explicit solutions of the hydrodynamic parameters in terms of axial ratio are now available, analytic inversion procedures are not.
The principles of two numerical inversion procedures have been outlined before [2,3]. A given hydrodynamic parameter has a line solution of the two axial ratios ( $a / b, b / c$ ) characterizing a general ellipsoid of semi-axes $a \geqslant b \geqslant c$. Hence if two or more are combined graphically a unique solution may be found from the intersection. The parameters would thus be chosen according to how 'orthogonal' their intersection was, their experimental measurability and their sensitivity. These criteria however proved very restrictive and the only generally applicable method was one involving intersection of the $R$ function (derived from viscosity and sedimentation measurements) with $\delta_{ \pm}$functions (derived from viscosity and the two electric birefringence decay constants, $\theta_{+} \theta_{-}$) [2, 4]. Even here, hitherto available methods for extraction of the two decay constants from a two-term exponential decay were impossible with data of current experimental precision. However, it was shown that a new method, where information from the $R$ function (which can be relatively easily determined) is placed in the analysis for the extraction of the decay constants as a constraint provided adequate resolution for data of current experimental precision. We now present the FORTRAN IV algorithm on which this method is based.
The alternative method [3] is to combine $R$ graphically with the $\Lambda$ function (determined from viscosity and harmonic mean relaxation data). This method is not generally applicable to all macromolecules but only to those asymmetric enough (one axial ratio $\gtrsim 3$ ) so that the $\Lambda$ function is sufficiently sensitive but not so asymmetric that the measured harmonic mean relaxation time is not affected by internal rotations within the macromolecule. However, because this method is simpler we present its algorithm briefly first.


Fig. 1. Flow chart for the $\Lambda-R$ algorithm.

## 2. A SIMPLE GRAPHICAL INVERSION PROCEDURE

The essence of the procedure is described in the flow chart of Fig. 1. The value of $\Lambda$ or $R$ for any specified value of the pair of axial ratios $(a / b, b / c)$ can be evaluated numerically [1] using a standard numerical package for solving the elliptic integrals. Arrays of such values are evaluated in the $(a / b, b / c)$ plane (a $21 \times 21$ matrix takes approximately 1000 s of computer time in a CDC cyber 72). A contour plotting routine ('CONTRL' in the CDC GHOST graphics system) interpolates between these matrix points and can plot the $\Lambda$ and $R$ functions in the $(a / b, b / c)$ plane.

## 3. AN R-CONSTRAINED LEAST SQUARES ALGORITHM

This algorithm is more complicated and it will be instructive to present it in some detail. The problem revolves around extracting the two decay constants for an asymmetric particle


Fig. 2. Flow chart for the $R$-constrained least squares algorithm.
from an electric birefringence decay curve. The resolution of exponentials is notoriously difficult even for very precise data [5, 6] - this is clearly illustrated in Fig. 1 of Small and Isenberg [7]. A consideration of two recent papers by Jost and O'Konski [5], and O'Connor et al. [6] reveals that, for a two-term exponential decay a non-linear least squares method is the most applicable. Even so, the requirements on the precision of the experimental birefringence data are about two orders of magnitude greater than the current limits $[2,8]$. The procedure introduced before [2] was to include information from the parameter $R$ as a


Fig. 3. Plot of the $R$-function for a hypothetical protein of axial ratio $(a / b, b / c)=(1.5,1.5)$. The coordinates of the encircled points are used for cubic spline interpolation in the $R$-constrained least squares algorithm.
constraint in the analyses. In this way the problem is effectively reduced from four independent variables (two pre-exponential factors $A_{ \pm}$and two decay constants $\theta_{ \pm}$) to three $\left(A_{ \pm}^{\prime}, a / b\right)$ since $a / b$ should now specify a unique value for $b / c$, and hence $\theta_{ \pm}$.

## 4. COMPUTATIONAL METHOD

An outline of the procedure is given in the flow chart of Fig. 2. The $R$ function is assumed to have already been measured from the ratio of the sedimentation concentration regression coefficient to the intrinsic viscosity. It is then plotted in the $(a / b, b / c)$ plane over a suitable range of axial ratio (see Section 2 above). The coordinates of 'knots' in the curve (Fig. 3) can then be specified in our routine (or alternatively if the facility is available the whole $R$-curve can be digitized). Other preliminary data required for converting a given estimate for ( $a / b$, $A_{+}^{\prime}, A_{-}^{\prime}$ ) into decay constants through the $\delta_{ \pm}$functions are the intrinsic viscosity, solvent viscosity, molecular weight and temperature of the birefringence experiment.

The program (Table 1, with key to computer symbols given in Table 2) employs the NAG quasi-Newtonian algorithm E04JAF [9] for minimising a function $F$, subject to bounds on the estimates for the independent variables. The subroutine FUNCTI (Table 3) specifies $F$ as the sum of the squares of the residuals for each current estimate of $\left(a / b, A_{+}^{\prime}, A_{-}^{\prime}\right)$ : the value of the axial ratio $b / c$ corresponding to a given estimate for $a / b$ is first evaluated with the aid of the cubic spline interpolation routine E01LF1 $\dagger$ applied to the $R$ 'knot' points introduced earlier. The value for $(a / b, b / c)$ specifies a unique value for the swelling independent hydrodynamic shape functions $\delta_{ \pm}$, which can be evaluated with the aid of the NAG numerical integral routine D01AGF. Using the values for the intrinsic viscosity, molecular weight, solvent viscosity and temperature of the birefringence experiment entered by the programmer, the routine will then evaluate the birefringence decay constants $\theta_{+}$from equation (4) of Harding and Rowe [2]. Hence the computer estimate for the decay $\stackrel{ \pm}{\text { curve }}$

$$
\Delta n=A_{+}^{\prime} \mathrm{e}^{-6 \theta+t}+A_{-}^{\prime} \mathrm{e}^{-6 \theta_{--}}
$$

is specified, and hence the sum of the squares of the residuals (ssr).

Table 1. Main program for the $R$-constrained algorithm. The sections denoted $\|$ correspond to the generation of synthetic data (cf. [2]).

```
C ************
C ******ETN*\frac{1}{#*}
C LINEAR TIME INCREASE, 100PTS.
C CUT OFF TIME: 10ONS
C STREAM OF RANDOM NUMBERS: ?
C O.1 OEG STANDARD ERROR ON EACCH DATA PT.
PROGRAM MAIN(INPUT,OUTPUT,TAPE2=INPUT,TAPE3=OUTPUT)
    COMMON/PARAM/GAMMA(101),T(101),A,C,D,NN,AA(6), AD(5)
    REAL R(101)
    REAL AA1,AA2,AA3,AA4,AA5,AA6,AD1,AD2,AO3,AD4,AD5,AD6
    REAL BL(3),BU(3),X(3),F,H(39)
    INTEGER IBOUND,IFAIL,J,LIW,LW,N
    INTEGER IH(5)
    REAL Q1,Q2,Q3,Q4
    WRITE (3,38)
    38
    +100NS, 100PTS")
    HRITE (3,39)
    39 FORMAT (
    +STREAM 3*)
    P=-1.1
    0021 I=1,101
    P=P+1.1
    R(I)=P
        T(I) =R(I)*1.0E-09
    R(I)=T(I)*1.0E09
    21 CONTINUE
C GOS8AF(O.X) SPECIFIES THE XTH STREAM OF THE RANDOM NUMBERS
    CALL GO5BAF(0.3)
    0050 I=1,101
C CALCULATE THE UNPERTURBED DECAY CURVE
    GAMMA(I)=0.07*EXP(-T(I)*5.0*5.815383E06) +
    +0.05*EXP(-T(I) #6.0F4.1564612EO6)
C NOW PERTURB EACH OF THE IOO DATA POINTS USING A NORMAL PSEUDO RANDOM
C NUMBER GENERATOR GOSADF
        GAMMA (I)=GAMMA(I) +((1.74555E-03)*GO5ADF(Y))
        50 CONTINUE
C REAO IN THE VALUES FOR THE LOWER LIMITS FOR THE INITIAL GUESSES OF THE
C A/B, A+, A-, THE LOWER (L) ANO UPPER (U) LIMITS FOR THE COMPUTER
C ESTIMATES, THE COORDINATES OF THE A/B KNOT VALUES ANO THEN THE
C COOROINATES OF THE B/C VALUES FOR THE R-CURVE TO WHICH THESE
C ESTIMATES ARE CONSTRAINED
    READ(2,*)XX1,XX2,XX3,BBL1,8BL2,BBL3,83U1,BBU2,BBU3,
    +AA1,AA2,AA3,AA4,AA5,AA5,AO1,AD2,AD3,AD4,AD5,AD6
        AA(1)=AA1
        AA(2) =AAL
        AA(3)=AA3
        AA(4)=AA4
        AA(6)=AAG
        AD(1) =AD1
        AO(2)=AD?
        AD(3)=AD3
        AD(4) =AD4
        AD(5)=AD5
        AO(5)=ADG
        N=3
        IBOUNO=0
        Q1=1.0
C SCALE UP A+ AND A- (SEE NAG MANUAL)
        x424=x 22}*100.0
        010 I=1,3
C GENERATE STARTING ESIIMATES FOR A/B, A+ AND A-
        7=G05AAF (XI
        x(1)=x\times1+0.2*2
        x(2) =x x2+2.0* %
        x(3)=x\times3+2.0*)
        BL(1)=B3L1
        BL(2)=BBL
        BL(3)=B3L3
        BU(1)=BBU1
        BU(2)=BBU2
        BU(3)=BBU3
        LIW=5
        LW=39
        IFAIL=1
        CALL EOLJAF(N,IBOUNO,RL,BU,X,F,IW,LIW,W,LW,IFAIL)
        IF(IFAIL.NE.OI WRITE (3,100)IFAIL
        IF(IFAIL.EQ.1)GOTO 20
        100 FORMAT ("ERROR EXIT TYPE*,I3,"SEE ROUTINE MANUAL*`)
C SCALE BACK DOWN AGAIN A+ ANO A-
        x(2)=x(2)*.01
        x(3)=x(3)*.01
        WRITE(3,110)F
```

```
        WRITE(3,120)(X(1),X(2),X(3))
110 FORMAT(*GUNCTION VALUE ON EXIT IS**F15.12)
120 FORMAT(.*A/B=*,FR.5.* A+=*,F15.12.
        4** A-="",F1S.12)
        +"* A-=",F15.12)
        Q1=F
        Q2=x(1)
        Q3=x(2)
        04 =x(3)
    30 CONTINUE
        WRITE (3,130)
130 FORMAT!
        FORMAT (1.4%)
140 FORMAT
    10 CONTINUE
        WRITE (3,150)QQ1
150 FORMATY QEST LEAST SQUARES VALUE = *,F15.12)
        WRITE (3,160)02
160 FORMAT ?:"
        WRITE (3,170)Q3
        M WRITE (3,170)Q3
        WRITE (3,180)\3
180 FORMAT( WRIGE(3,190)\4
180 FORMAT(, WRITE\ 3,190)\4
    20 STOP
    STOP
        A/B}=**F6.5
        B/C=`,F8.5)
                                    A+=*,F7.4)
        FORMATY,
        A-=",F7.41
        WRITE (3,140)
```



## 5. RESULTS

In the main program (Table 1) we have incorporated a method for generating our own synthetic birefringence curve of mock random standard absolute error of 0.1 degrees, (within the limits of current experimental precision [8]) on each data point.

Owing to the possible danger of the routine falling into subsidiary minima [5] it is necessary to repeat the processing for several different initial starting estimates for the three independent variables. Provision for this is made in the program: the user enters the lower limit for the three parameters and the routine uses NAG pseudo-random number generator G05AAX to produce the initial estimates within reasonable limits.

Table 2. Key to computer symbols used*

| Computer Symbol | Parameter |
| :---: | :--- |
| $A . A / B$ | $a / b$ |
| $B$ | $b$ |
| $B / C$ | $b / c$ |
| $C$ | $c$ |
| $A_{+}$ | $A_{+}^{\prime}$ |
| $A_{-}$ | $A_{-}^{\prime}$ |
| GAMMA | Birefringence (radians) |
| $\dagger X(1)$ | Starting estimate for $a / b$ |
| $\dagger X(2)$ | Starting estimate for $A^{\prime}$ |
| $\dagger X(3)$ | Starting estimate for $A^{\prime}$ |
| $X C(1)$ | Current estimate for $a / b$ |
| $D$ | Value of $b / c$ corresponding to this estimate |
| $S$ | Value of $v$ corresponding to this estimate |
| $V$ | Value of $\delta_{+}$corresponding to this estimate |
| $W$ | Value of $\delta_{-}$corresponding to this estimate |
| THPLUS | Value of $\theta_{+}$corresponding to this estimate |
| THMNUS | Value of $\theta_{-}$corresponding to this estimate |
| $X C(2)$ | Current estimate for $A_{+}^{\prime}$ |
| $X C(3)$ | Current estimate for $A_{-}^{\prime}$ |
| AA1-AA6 | $a / b$ coordinates for 6 pts on the $R$ curve |
| AD1-AD6 | $b / c$ coordinates for 6 pts on the $R$ curve |
| $Q$ | square of a residual |
| $F C$ | sum of squares of the residuals (ssr) |

[^0]Table 3. Subroutine for evaluating the sum of the squares of the residuals for a given estimate of $a / b$, $A_{+}^{\prime}$ and $A_{-}^{\prime}$

```
C SUBROUTINE FOR CALCULATING THE SUM OF THE SQUARES OF THE RESIOUALS FOR
C CURRENT ESTIMATES OF A/B, At ANO A-
C KB = BOLTZMANNS CONSTANT, NA = AVOGADROS NUMBER
    SUBROUTINE FUNCT1 (N,XC,FC)
    COMMON/PARAM/GAMMA(101),T(101),A,C,D,NN,AA(6), AD(5)
    EXTERNAL FUN
    REAL Q,FC
    INTEGER N
    OIMENSION ALPHA(9)
    REAL XC(N)
    REAL <2, <3
    REAL THPLUS,THMNUS,TEMP,ETA,M,O,P,KB,NA,MW
    NN=0
    A = XC(1)
    NM=6
    IEXIT=0
C CALL LIBRARY ROUTINE FOR THE CUBIC POLYNOMIAL FIT TO THE R-CURVE POINTS
C A LISTING OF THIS IS GIVEN BELOW
    CALL EO1LFI(NM,AA,AD,A,D,IEXIT)
    C=1.0/D
    B=1.0
    DO45 K=1,9
    AZ=0.0
    B7=1000000
    NN=NN+1
    MAXDIV =50
    EPS=1.OE-08
    ACC=0.0
    IFAIL=0
    CALL DOIAGF(AZ,BZ,FUN, MAXOIV,EPS, ACC, ANS, ERROR,NOFUN,IFAIL)
    ALPHA (NN) = ANS
    45 CONTINUE
    S=(1.0/(A*B*C))*((4.0/15.0)*((ALPHA(7) +ALPHA(B)
    + +ALPHA(9))/(ALPHA(8)*ALPHA(9)+ALPHA (9)*ALPHA
    +(7)+ALPHA(7)*ALPHA(8)))+(1.0/5.0)*((1ALPHA(2)
    * +ALPHA(3))/(ALPHA(4)* (B*B*ALPHA(2) + C*C*ALPHA(3)
    * 1))+((ALPHA(3)+ALPHA(1))/(ALPHA(5)* (C*C*ALPHA(3)
    + +A*A*ALPHA(1))))+((ALPHA (1)+ALPHA (2))/(ALPHA(6)
    + *(A*A*ALPHA(1)+B*B*ALPHA(2)))))
        M=(B*B+C*C)/(B*B*ALPHA(2)+C*C*ALPHA(3))
        O=(C*C+A*A)/(C*C*ALPHA(3)+A*A*ALPHA(1))
        P=(A*A+B*B)/(A*A*ALPHA(1)+B*B*ALPHA(2))
        Z=((A* B*C)/(12.0))*(()(1.0/M)+(1.0/0)+11.0/P
    + )}=(((1.0/M**2.0)+(1.0/0**2.0)+(1.0/P**2.0))
    +((1.0/(M*O))+(1.0/(0*D))+(1.0/(D*M
    + Jj)**0.5i)
    U=((A*B*Ci)}(12.0))*(()(1.0/4)+(1.0/0)+(1.0/
    + 1)+(((1.0/M**2.0)+(1.0/0**2.0)+(1.0/0**2.0))-
    +((1.0/(M*0))+(1.0/(0*D))+(1.0/(P*M
    + i)j;*0.5ij
        V=6.0*U*S
        W=6.0*Z*S
C ENTER INTRINSIC VISCOSIIV
C ETA=2.74GORERATURE
TEMP=293.0
C ENTER MOLECULAR WEIGHT
    MW=71744.0
    KB=1.38046E-16
    NA =6.0248E23
    ENTER SOLVENT VISCOSITY
    SOLV=.01
    THPLUS=(NA*KB/(SOLV* 6.0))*(TEMP/(ETA*MH))**
    THMNUS=(NA*KB/(SOLV*5.0))*(TEMP/(ETA*MH))*W
    x2 = xC (2)
    x3=xC (3)
    FC=0.0
        0075 I=1,101
        Q=(GAMMA(I) - (0.01* X2*EXP(-5.0*THPLUS*T(I))+0.01*X3*EXP
    +(-6.0*THMNUS*T(I))\)**2.0
    FC=FC+Q
    75 CONTINUE
    RETURN
    ENO
```

Despite the need for these precautions it is evident from a simulation for a typical globular protein of true axial ratios $(a / b, b / c)=(1.5,1.5)$ that the algorithm is extremely stable (Table 5).

The algorithm has also been tested for the effect of error in the intrinsic viscosity and molecular weight, for different true axial ratios and for different true pre-exponential factors and in every case remains stable. In order to achieve the highest accuracy with the method it is

Table 4. Subroutine for specifying the integrands in the numerical evaluation of the elliptic integrals

> (cf. [1])

```
C SUBRGUTINE FOR CALCULATING THE ELLIPTIC INTEGRALS USED FOR DETERMINING
C THE S VALUE FROM THE CURRENT ESTIMATE FOR A/B
    PEAL FUNCTION FUN(Y)
    COMMON/OARAM/GAMMA(101),T(101),A,C,O,NN,AA(6),AD(5)
    B=1.0
    COT0(10,20,30,40,50,60,70,80;90),NN
    10 FUN=1:0'((A*A+Y)**1:5*(B*B+Y);**O:J*(C*C+Y)**0.5)
    PETURN
    20 FUN=1.0/((A*A+Y)**0.5*(B*B+Y)**1.5*(C*C+Y)**0.5)
    30 FUN=1.0/((A*A+Y)**0.5*(B*B+Y)**0.5*(C*C+Y)**1.5)
        RETURN
    40 FUN=1.0/((A*A+Y)**0.5*(B*B+Y)**1.5*(C*C+Y)**1.5)
    RETURN
    50 FUN=1.O/((A*A+Y)**1.5*(B*B+Y)**0.5*(C*C+Y)**1.5)
        RETURN
    60FUN=1.0/((A*A+Y)**1.5*(B*B+Y)**1.5*(C*C+Y)**O.5)
    REIURN
    70 FUN=Y/((A*A+Y)**0.5*(B*B+Y)**1.5*(C*C*Y)**1.5)
    RETURN
    80FUN=Y/((A*A+Y)**1.5*(B*B+Y)**0.5*(C*C+Y)**1.5)
    PETURN
    90 FUN=Y/((A*A+Y)**1.5*(B*B+Y)**1.5*(C*C+Y)**0.5)
    RETURN
    END
```

necessary to develop procedures for determining the optimum cut-off time for the birefringence decay and also to allow for the concentration dependence of the decay constants; these have already been outlined [2].

## SUMMARY

Two methods are now available for modelling biological macromolecules in solution as tri-axial ellipsoids. Both involve numerical inversion of swelling-independent hydrodynamic shape functions followed by graphical intersection of two or more of these. The necessary computational procedures on which these methods are based are presented here. The first involves data from fluorescence depolarization, viscosity and sedimentation velocity but is applicable only to a restricted class of particle asymmetries. The second involves data from electric birefringence, viscosity and sedimentation velocity, and although more generally applicable, requires constraints in the minimization procedure for extracting the relevant birefringenece decay parameters.

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Table 5. Results for a synthetic protein (cf. [2]) of true axial ratio $(a / b, b / c)(1.5,1.5)$, true $A_{+}^{\prime} 0.07$ and true $A^{\prime}-0.05 \mathrm{rad}$

```
PROTEIN 1, 0.1 DEG. ABSOLUTE ERROR
```

FUNCTION VALUE ON EXIT IS 000399962998
$A / B=1.48309 A_{A}=$. 070458728408 A $^{2}=.048831535604$
FUNCTION VALUE ON EXIT IS $\quad 000399962998$
A/B


FUNCT ION VALUE ON EXIT IS $\quad .00399962998$
$A / B=1.48309$
$A+=\quad .070458881237$
$A-=$

BEST LEAST SQUARES VALUE $=.000399962998$
1.48309
. 0707
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#### Abstract

About the Author-Dr Harding graduated in Physics and Molecular Biophysics from Oxford in 1976. In 1977 he worked at the Atomic Energy Research Establishment, Harwell, Oxfordshire, receiving an $\mathrm{M} . \mathrm{Sc}$. for his work on the improvement in resistance to wear of ion implanted materials. From 1977 to 1980 he researched on modelling macromolecules in solution at the Department of Biochemistry, Leicester University, from where he received his Ph.D. He is now working at the University of Bristol on physico-chemical studies of bronchial glycoproteins.


[^0]:    * Other symbols are defined in the NAG manual [9] or ref [1].
    $\dagger$ On exit, $X(1), X(2), X(3)$ contains the best estimates for these parameters.

